## **Tracking Of Multiple Auvs in Two Dimensional Plane**

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ABSTRACT: Formation control using a leader-follower approach is a advancement in AUV technology for control and formation of multiple Autonomous underwater vehicles. This approach leads the other approaches of formation control like behaviour-based method, virtual structural method, artificial potentials as the theoretical formalization and mathematical analysis of these approaches are difficult and consequently it is not easy to guarantee the convergence of the formation to a desired configuration. On the other hand in the leader-follower approach, a robot of the formation, designated as the leader, moves along a predefined trajectory while the other robots, the followers, are to maintain a desired distance and orientation with respect to the leader. Numerical simulations are carried out to illustrate the effectiveness of the proposed formation scheme.

**Keywords:** Multiple AUV system, Formation control, Kinematics, Dynamics, Leader, Follower.

#### I. INTRODUCTION

An autonomous underwater vehicle (AUV) is a robot which travels underwater without requiring input from an operator. With the increase in technology and applications of AUV in different areas lots of attentions have been paid to the research on the cooperative control and formation control of multiple autonomous agents, especially on the cooperative control of groups of robots. History says that In 1987, Reynolds introduced a distributed behavioural model for flocks, herds and schools [6] where the three heuristic rules that of flock centring, collision avoidance and velocity matching were also introduced. In [6], each of dynamic agents was considered as a certain particle system whose dynamics can be expressed as a simple second-order linear equation. Furthermore, this kind of dynamic agents (particles) model was used in many of the following researches [4], [10]. Soon It was realized that multiple autonomous agents can be used to carry out more complicated jobs for single agent hard to finish. The recent advances in sensing, communication and computation enable the conduct of cooperative missions.

In many applications, a given task is too complex to be accomplished by a single robot; thus a multi-robot system working cooperatively is required to complete the job. Multi robot systems are more robust as compared to the single-robot systems because a team of robots provides certain amount of redundancy, which is useful when some of the robots malfunction also less time is needed to complete the job e.g. the use of AUVs for offshore operations includes ocean sampling, minesweeping, ocean floor survey, and oceanographic data collection. Instead of a single specialized expensive AUV, it is beneficial to use comparatively simple and inexpensive AUVs to cooperatively increase the service area.

In this paper the leader-follower formation control can be achieved as the leader AUV has to track the desired trajectory and the follower AUV tries to maintain a desired distance and angle relative to the leader. When all vehicles are in expected positions, the desired formation is established.

#### II. MODELLING OF AUV'S

To study the motion of marine vehicle 6 degrees of freedom are required since to describe independently the complete position and orientation of the vehicle we require 6 independent coordinates.[8] To describe position and translation motion first three sets of coordinates and their time derivatives are required. While for orientation and rotational motion last three sets of coordinates and their time derivatives are required. Table I shows this DOF.

TABLE I NOTATION USED FOR AUV MODELLING

DOF	Motion	Forces	Linear nd angular velocity	Postio n
1	Motion in X- direction(surge)	X	u	X
2	Motion in Y- direction(sway)	Y	V	У
3	Motion in Z- direction(heave	Z	W	z
4	Rotation about X- axis(roll)	K	p	Ø
5	Rotation about Y- axis(pitch)	M	q	θ
6	Rotation about Z- axis(yaw)	N	r	Ψ

To obtain a mathematical model of the AUV, its study can be divided into two sub-categories: Kinematics and Dynamics.

Kinematics deals with bodies at rest or moving with constant velocity whereas dynamics deals with bodies having accelerated motion

#### III. AUV KINEMATICS AND DYNAMICS

To study the planar motion, we define an inertial frame {I} and a body fixed frame {B}. The origin of {B} frame coincides with the AUV centre of mass (CM) while its axes are along the principal axes of inertia of the vehicle.

www.ijmer.com Vol.2, Issue.6, Nov-Dec. 2012 pp-4119-4121

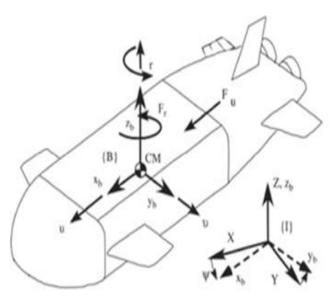


Fig. 1 AUV diagram showing inertial and body fixed frames

 $X_b$  is the longitudinal axis,  $Y_b$  is the transverse axis, and  $Z_b$  is the normal axis. The kinematic equations of motion for an AUV on the horizontal X-Y plane can be written as

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{w} \end{bmatrix} = \begin{bmatrix} \cos(\Psi) & -\sin(\Psi) & 0 \\ \sin(\Psi) & \cos(\Psi) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} u \\ v \\ r \end{bmatrix}$$

(linear) surge (forward) and sway (side) velocities, respectively, defined in the body fixed frame. The orientation of the vehicle is described by angle  $\Psi$  measured from the inertial X-axis and r is the yaw (angular) velocity. Assuming that (i) the CM coincides with the centre of buoyancy (CB) (ii) the mass distribution is homogeneous, (iii) the hydrodynamic drag terms of order higher than two are negligible, and (iv) heave, pitch and roll motions can be neglected, the dynamics is expressed by the following differential equations:

$$\dot{u} = \frac{m_{22}}{m_{11}} vr - \frac{X_u}{m_{11}} - \frac{X_{u|u|}}{m_{11}} + \frac{1}{m_{11}} F_u$$

$$\dot{v} = \frac{m_{11}}{m_{22}} ur - \frac{Y_v}{m_{22}} v - \frac{Y_{v|v|}}{m_{22}} + \frac{1}{m_{22}} F_v$$

$$\dot{r} = \frac{m_{11} - m_{22}}{m_{33}} uv - \frac{N_r}{m_{33}} r - \frac{N_{r|r|}}{m_{33}} + \frac{1}{m_{22}} r|r|$$

The variable  $F_u$  denotes the control force along the surge motion of the vehicle and variable  $F_v$  denotes the control force along the sway motion of the vehicle. Third equation is uncontrolled and the AUV is an underactuated dynamic system. The constants  $m_{11}$  and  $m_{22}$  are the

combined rigid body and the added mass terms, and  $m_{33}$  is the combined rigid body and added moment of inertia about  $Z_b$  axis.  $X_u,\ X_{u|u|}$ ,  $\ Y_v,\ Y_{v|v|},\ N_r$  and  $N_{r|r|}$  are the linear and quadratic drag terms coefficients.

ISSN: 2249-6645

# IV. REFERENCE PATH AND CONTROLLER DESIGN

We choose a reference circular inertial planar trajectory given as follows

$$Xr(t) = 8sin(0.01t) m$$
,

$$Y_r(t) = 8\cos(0.01t) \text{ m}.$$

From this reference path, we find the error in position actual position – reference position). This error is then given to proportional derivative controller (PD controller) which generates necessary controlling signals. The output from controller is then feed to system (AUV) which reduces the error in position and thus, AUV tracks the desired trajectory. The reference path for follower AUV is the circle with same frequency but with different radius

#### V. SIMULATION NUMERICAL DATA'S

Here some numerical data's are considered for simulation

Mass (M)-185 Kg

Rotational mass  $I_Z$  - 50 kgm<sup>2</sup>

Added mass  $X_{ii}$  - 30 Kg

Added massY<sub>v</sub> - 80 Kg

Added mass  $N_{\dot{r}}$  - 30 kgm<sup>2</sup>

Surge linear drag X<sub>u</sub> -70 kg/s

Surge quadratic drag  $X_{u|u|}$  - 100 kg/m

Sway linear drag  $Y_v$  - 100 kg/s

Sway quadratic drag  $Y_{\nu|\nu|}$ - 200 kg/m

Yaw linear drag N<sub>r</sub> - 50 kgm<sup>2</sup>/s

Yaw quadratic N<sub>r|r|</sub> -100 kgm<sup>2</sup>

Also, m<sub>11</sub> = m -  $X_{\dot{u}}$  = 215 kg, m<sub>22</sub> = m -  $Y_{\dot{v}}$  = 265 kg, m<sub>33</sub> = m -  $N_r$  = 80 kgm<sup>2</sup>

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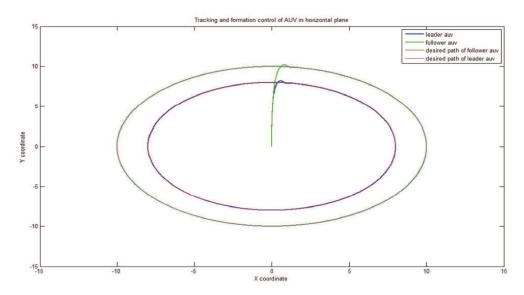


Fig 2. Tracking and formation control of AUVs in horizontal plane

The leader AUV is tracking its desired path which is a circle of radius 8m and also the follower AUV is maintaining a constant distance of 2m from the leader AUV.

#### VI. CONCLUSIONS

In this paper modelling of AUV is done and kinematics and dynamic equations of motion were obtained. Through simulation of this model we obtain a stable formation scheme for multiple AUV system, Therefore, for the simplification purpose, only formation of the vehicles in horizontal plane not in 3D plane and without obstacle avoidance is considered in this paper. However, from the design procedure presented in this paper, it is not difficult to find that if we add another potential term, which is similar to the one of form, then in future the other issues also can be handled with the proposed formation scheme.

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