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Application of PWM Control Strategy on Z-Source Isolated Dual active bridge DC-DC Converters

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Abstract: *This project presents a Z-source with bidirectional dc–dc converter. The switching count is reduced by adding a passive element. Thus, we are improving the output voltage level. The voltage regulation range of proposed converter is better than that of the traditional bidirectional dc–dc converter. The fully bridge symmetrical circuit configuration, is neither a high-voltage side nor a low-voltage side in the circuit structure, and the sources connected to the dc side of each H-bridge circuit with voltage sources and current sources. This method can reduce current stress and improves the system efficiency.*

In this paper we are presenting a dual active bridge (DAB) dc–dc converter is also known as Bidirectional DC-DC converter. Both simulation results are shown by using MATLAB software.

Index Terms: *Bidirectional dc–dc converter (BDC), coordinated control, double-closed loop, Z-source.*

I. Introduction

Bidirectional DC–DC converter (BDC) is a dual active bridge converter. It is a two quadrant operating dc–dc converter. Nowadays, the need for electric power is increased. Hence there is a need to implement bidirectional dc-dc converters.

Because of the features of saving in volume, weight, and cost, it has been widely used in applications such as dc motor driving systems, uninterruptible power supplies (UPSs), battery charging and discharging systems, and auxiliary power supplies for hybrid electrical vehicles where the function of bidirectional power flow is required. Generally, BDC is divided into two types: non insulated type and insulated type.

In addition, the isolated BDC (IBDC) is needed to provide absolute electrical isolation between the primary side and the secondary side for protecting the equipment and operators IBDC is usually based on the single phase and H-bridge topology with an isolation transformer.

Fig. 1 shows a typical configuration of Bidirectional DC-DC converter. From the aspect of circuit structure, it has the following points are: 1) The high-frequency transformer provides the required isolation and voltage matching between two voltage levels; 2) transformer voltage ratio is not one, and both sides of the circuit are defined as the high-voltage side compared to the low-voltage side, which makes the installation location of power sources for both sides not interchangeable; 3) the sources connected to the dc side of each H-bridge can only be voltage sources; and 4) the transformer's leakage inductance serves as the instantaneous energy storage device.

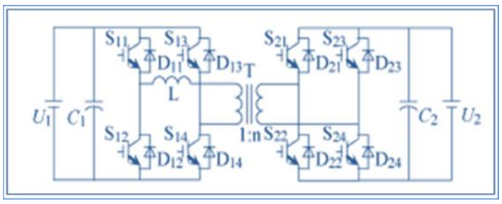

Fig.1 Schematic of the DAB dc–dc converter

This paper presented a Bidirectional DC-DC converter is also known as dual active bridge (DAB) dc–dc converter. We presented a Z-source with bidirectional dc–dc converter by reducing the switching count by adding an passive elements we are going to increases the output voltage level, Comparing with the traditional bidirectional dc–dc converter, the proposed converter has an wider regulation range of voltage and many application based converter for hybrid vehicles and for any hybrid application. The fully bridge symmetrical circuit configuration, is neither a high-voltage side nor an low-voltage side in the circuit structure, and the sources connected to the dc side of each H-bridge circuit with voltage sources and current sources. This method can reduce current stress and improves the system efficiency.

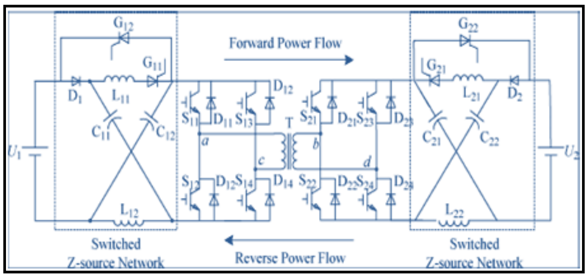

Fig.2 Schematic circuit of a Z- sources with bidirectional dc–dc converter

II. Theoretical Model of Dab Converter

A. Basic Principle of Operation

Fig. 1 consists of two full-bridge circuits connected through an isolation transformer and a coupling inductor *L*, which may be provided partly or entirely by the transformer leakage inductance. The full bridge on the left hand side of Fig. 1 is connected to the HV dc bus and the full bridge on the right hand side is connected to the low-voltage (LV) side. Each bridge is controlled to generate an HF square-wave voltage at its terminals. By incorporating an appropriate value of coupling inductance, the two square-waves can be suitably phase Shifted with respect to each other to control power flow from one dc source to another. Thus, bidirectional power flow is enabled through a small lightweight HF transformer and inductor combination, and power flows from the bridge generating the leading square-wave. Although various modes of operation of the DAB converter have been presented for high power applications the square-wave mode is supposedly the best Operating mode.

This is because imposing quasi-square-wave on the transformer primary and secondary voltages results in trapezoidal, triangular, and sinusoidal waveforms of inductor current in the bidirectional DC-DC converter. These modes are beneficial for extending the low-power operating range of the converter. Although these modes tend to reduce the switching losses, the voltage loss is significant due to zero voltage which reduces the effective power transfer at high-power levels. The key operating waveforms of the converter during buck mode, i.e., when power flows from the HV side to the LV side are shown. The voltages generated by the two full bridges, *V*HV on the HV side and *V*LV on the LV side, are represented as square-wave voltages with 50% duty cycle. But proposed circuit is with Z sources network i.e Switched Z-sources bidirectional DC-DC converter

B. Boost Model

According to the analysis, the upper and lower devices of each phase leg in both H-bridges can be gated on simultaneously, so its reliability is improved greatly. Furthermore, the shoot-through zero state brings the boost ability to the Z sources We also take the forward power flow as an example to analyze. Assuming that the inductors *L*11 and *L*12 and capacitors *C*11 and *C*12 have the same inductance and capacitance, respectively, the Z-source network becomes symmetrical. From the symmetry and the equivalent circuits, we have (3)

$$U_{C11} = U_{C12} = U_C \quad (1)$$

$$u_{L11} = u_{L12} = u_L \quad (2)$$

we have

$$u_L = U_1 - U_C \quad (3)$$

$$u_d = U_1 \quad (4)$$

$$u_i = U_C - u_L = 2U_C - U_1 \quad (5)$$

Where, *ud* is the dc-link voltage of the switched Z-source network and *ui* is the dc-link voltage of the H-bridge we have

$$\begin{aligned} u_L &= U_C \\ u_d &= 2U_C \quad (6) \\ u_i &= 0 \end{aligned}$$

Given that a switching cycle *T* of SZIBDC consists of two sections, *T*0 for the shoot-through zero state and *T*1 for the normal switch state and the open zero state, respectively, the average voltage of the inductor over one switching cycle should be zero in steady state; thus, from (3) to (8), we have

$$U_L = \overline{u_L} = [T_0.U_C + T_1.(U_1 - U_C)]/T = 0 \quad (7)$$

Where, T = T0 + T1, in which case (7) can then be expressed as

$$\frac{U_C}{U_1} = \frac{T_1}{T_1 - T_0} \quad (8)$$

In the normal switch state and the open zero state, by substituting (8) into (5), ui can be expressed as

$$u_i = \frac{T}{T_1 - T_0}U_1 = \frac{\pi}{\pi - 2\alpha}U_1 \quad (9)$$

Therefore, we have

$$u_i = \begin{cases} 0, \\ \pi/(\pi - 2\alpha)U_{1,} \end{cases} \quad (10)$$

C. Voltage Regulation Model

In the traditional Z-source inverter, the regulation of voltage is achieved by the modulation index *M* and boost factor *B* which is unfit for the PWM in the SZIBDC.

Considering this, this paper presents a phase-shifting shoot through control method. Combining with the analysis of Section II, the main waveforms of SZIBDC in phase-shifting shoot-through control are shown in Fig. 6, where the transformer voltage ratio is one, *S*0 is the shoot-through pulse, *uD*1 is the voltage of the diode *D*1, *u*ac and *u*bd are the voltages of the primary and secondary sides of the transformer, respectively, and *iL*11, *iL*12, and *iL*22 are the currents flowing through the inductors *L*11, *L*12, and *L*22, respectively. In the traditional phase-shifting control of the H-bridge, the converter is in the open zero state for an interval (*t*0–*t*2, *t*3–*t*5). By regulating the width of the interval during a switching cycle, the average output voltage can be stepped down. Additionally, from (12), if the shoot-through pulse (*t*1–*t*2, *t*4–*t*5) in the open zero state is added, the average output voltage can be stepped up. Note that the shoot-through zero states are evenly allocated into each phase and it does not change the total zero-state time interval. That is, the active states are unchanged.

III. Simulation Analysis

This paper presented a Z-source with Bidirectional DC-DC converter. We presented a Z-source with bidirectional dc–dc converter by reducing the switching count by adding an passive elements to improve the system efficiency, we are going to increases level of output voltage, Comparing with the traditional bidirectional dc–dc converter, the proposed converter has an wider regulation range of voltage and many application based converter for hybrid vehicles and for any hybrid application. The fully bridge symmetrical circuit configuration, is neither a high-voltage side nor an low-voltage side in the circuit structure, and the sources connected to the dc side of each H-bridge circuit with voltage sources and current sources. This method can reduce current stress and improves the system efficiency.

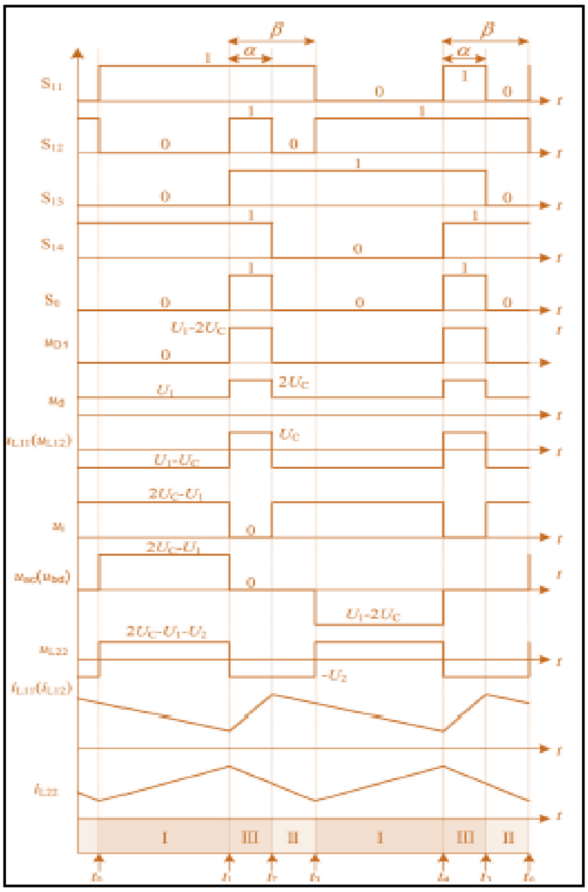

Fig.3 Main waveforms of SZIBDC in phase-shifting shoot-through control

A. Simulation circuit of an forward mode

Main Parameters of SZIBDC

In order to verify the correctness and validity of SZIBDC and its phase-shifting shoot-through bivariate coordinated control strategy, a simulation platform is established in electromagnetic transient simulation software Electro Magnetic Transients Including DC/Power System Computer Aided Design 4.2, and a laboratory prototype shown in Fig. 12 is constructed based on TMS320F2812 DSP. Furthermore, the main parameters of SZIBDC are as follows: inductors L11 = L12 = L21 = L22 = 0.1 mH, capacitors C11 = C12 = C21 = C22 = 220 μF, transformer voltage ratio n = 1, switching frequency f = 5 kHz, discretized values of a switching cycle N = 600, and input voltage U1 = 20 V.

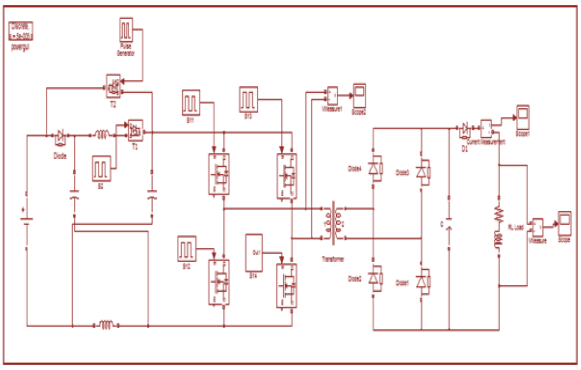
Fig 6.1 simulation arrangement for the proposed system in forward direction

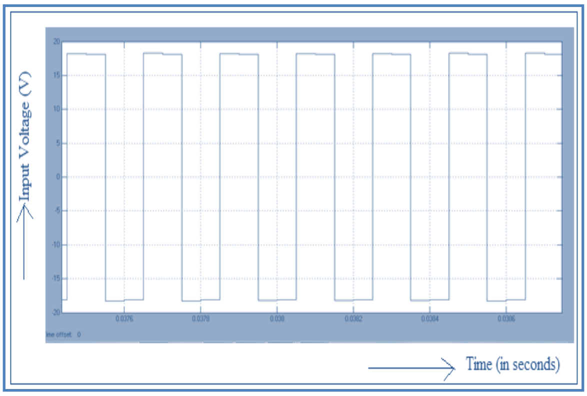

Fig 6.2 input side voltage of transformer in forward mode

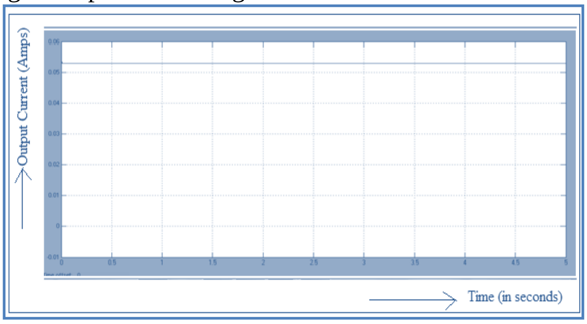

Fig 6.3 Output side current in forward direction mode

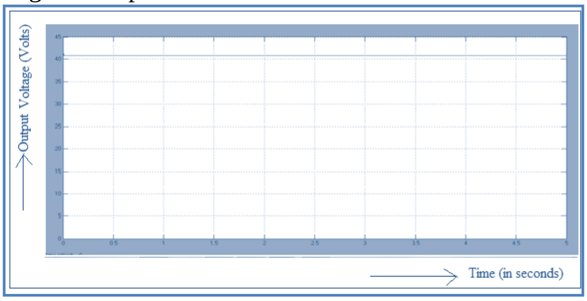

Fig 6.4 Output side voltage in forward direction mode

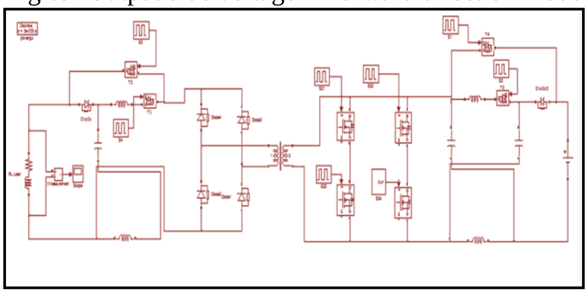

Fig 6.5 simulation arrangement for the proposed system in reverse direction

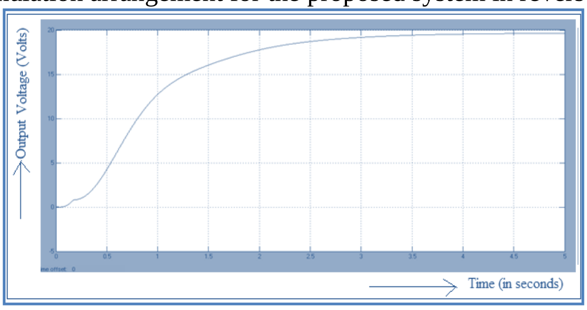

Fig 6.6 Output side voltage in reverse direction mode

B. Extinction of the work

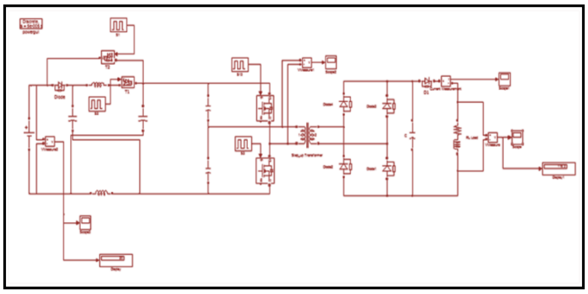

Fig 6.7 simulation arrangement for the proposed extinction of the system in forward direction

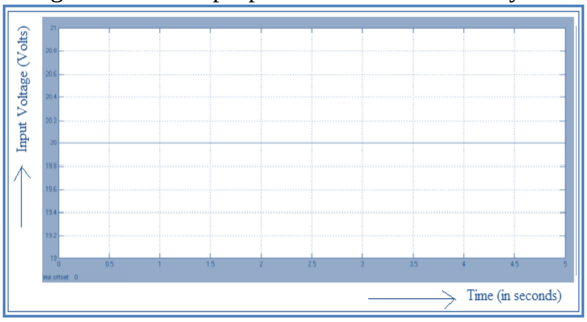

Fig 6.8 Input voltage waveform for the extinction of the system in forward direction mode

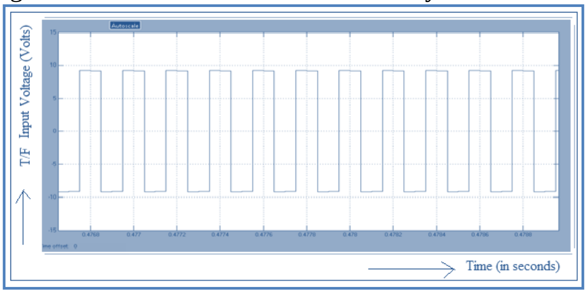

Fig 6.9 Transformer input voltage for the extinction of the system in forward direction mode

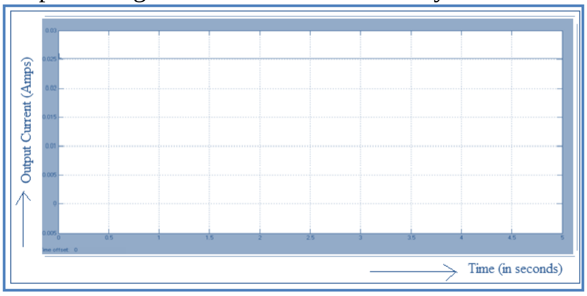

Fig 6.10 Output current waveform for the extinction of the work in forward direction mode

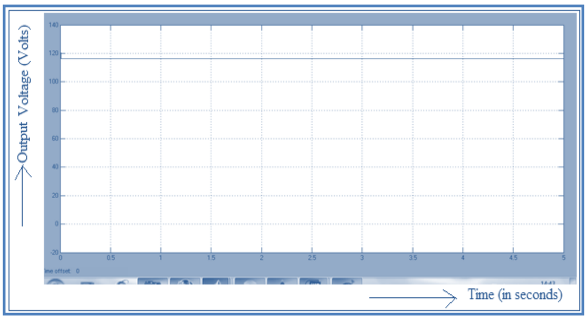

Fig 6.11 Output voltage waveform for the extinction of the system in forward direction mode

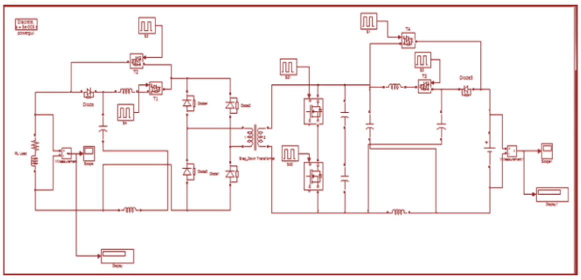

Fig 6.12 simulation arrangement for the proposed extinction of the system in reverse direction mode

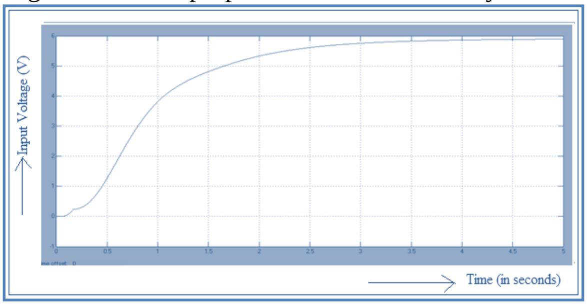

Fig 6.13 Input voltage for the extinction of the system in reverse direction mode

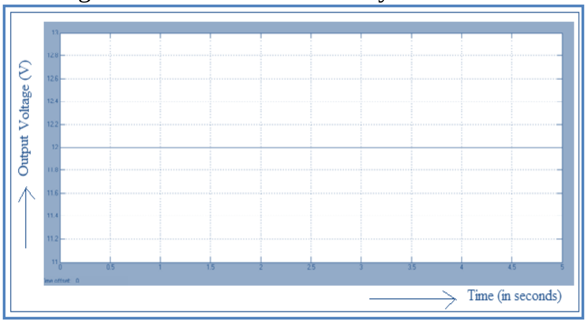

Fig 6.14 Output voltage waveform for the extinction of the system in reverse direction mode

C. Simulation Analysis

In simulation, SZIBDC is in open-loop control for an interval t = 0–0.5 s and in closed-loop control for an interval t = 0.5–2 s. The output voltage reference is given the values of 10, 40, and 10 V for three intervals t = 0.5–1 s, t = 1–1.5 s, and t = 1.5–2 s, respectively. Fig. 13 shows the simulation results for SZIBDC under different operating states. As can be seen from Fig. 13, in open-loop control (t = 0–0.5 s), $\alpha = \beta = 0$, and the output voltage is 19 V which approximately equals the input voltage. When t = 0.5 s, SZIBDC enters into bucking start-up closed-loop control (t = 0.5–1 s), and the output voltage reference is 10 V. Due to $\alpha = \beta = 0$ at this point, the control system works in control mode II, α remains zero and β increases, the output voltage decreases rapidly and stabilizes in 10 V after 0.04 s, and β stabilizes in 1.56 rad.

When t = 1 s, the output voltage reference jumps to 40 V, and SZIBDC jumps into boosting closed-loop control (t = 1–1.5 s). Due to $\beta > \alpha = 0$ at this point, the control system changes into control mode III, α remains zero and β decreases, and the output voltage increases. When t = 1.003 s, β decreased to be equal with α while the output voltage is lower than 40 V, the control system changes into control mode IV, α and β increase at the same speed, the output voltage increases rapidly and stabilizes in 40 V after 0.07 s, and α and β stabilize in 1.06 rad.

When t = 1.5 s, the output voltage reference jumps to 10 V again, and SZIBDC jumps into bucking closed-loop control (t = 1.5–2 s). Due to $\beta = \alpha > 0$ at this point, the control system changes into control mode I, α decreases and β remains constant, and the output voltage decreases. When t = 1.535 s, α decreases to zero while the output voltage is higher than 10 V, the control system changes into control mode II, β increases, the output voltage decreases rapidly and stabilizes in 10 V after 0.03 s, and β stabilizes in 1.56 rad. Note that the final state of the process is in line with the previous bucking start-up closed-loop control.

IV. Conclusion

In this project, by reducing the switching count and by adding a passive elements we improved the output voltage level of Z-sourced bidirectional dc–dc converter, Comparing with the traditional bidirectional dc–dc converter, the proposed converter has an wider regulation range of voltage. This method can reduce current stress and improves the system efficiency. Both the simulation results are checked by using MATLAB software.

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